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(72) Inventors:  
• Matsuoka, Hideo  
Nagoya-shi, Aichi 458-0044 (JP)  
• Okita, Shigeru  
Kawasaki-shi, Kanagawa 211-0025 (JP)

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(74) Representative: Coleiro, Raymond et al  
MEWBURN ELLIS  
York House  
23 Kingsway  
London WC2B 6HP (GB)

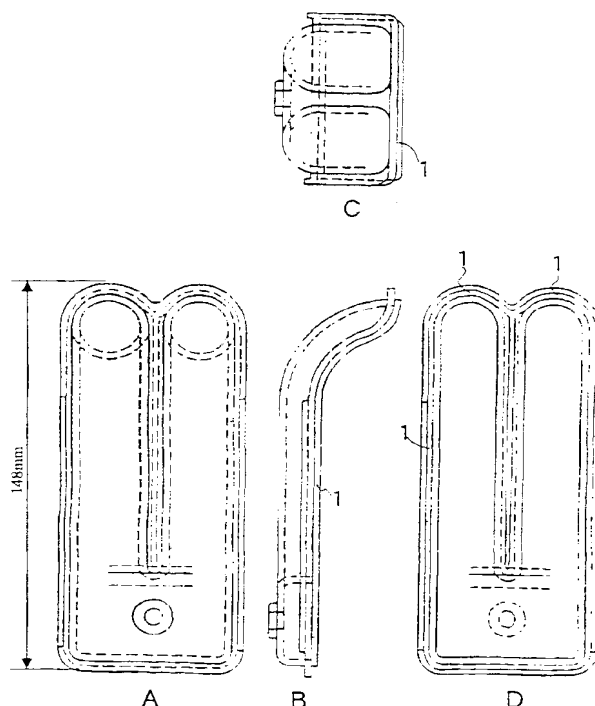
(71) Applicant: TORAY INDUSTRIES, INC.  
Tokyo 103-8666 (JP)

(54) Weldable polyamide resin compositions production thereof, and moulded products thereof

(57) A weldable resin composition which comprises  
100 parts by weight of nylon resin as component (A),  
0.1-50 parts by weight of polyolefin resin as component  
(B), 10-150 parts by weight of glass fiber as component

(C), 0-3 parts by weight of a copper compound as com-  
ponent (D) and 0-5 parts by weight of a silicone com-  
pound as component (E). A molded product may be pro-  
duced from the weldable resin composition by a welding  
operation such as vibration welding

FIG.1



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## Description

**[0001]** The present invention relates to a weldable resin composition which gives molded items superior in heat resistance, external appearance, dimensional stability, and uniform weldability. More particularly, the present invention relates to a weldable resin composition, a process for production thereof, and a molded item thereof, the resin composition being suitable for production of a hollow object by welding from two or more melt-molded items.

**[0002]** Nylon resin is widely used for automobiles and machine parts on account of its good moldability, heat resistance, toughness, oil and gasoline resistance, and wear resistance. The development of nylon resin in this field has been motivated mainly by substitution for metallic materials. Substitution actually proceeded from those parts in which nylon resin brings out its merit, such as weight reduction and corrosion prevention. With recent improvement in material performance and molding technology, nylon resin has reached a stage at which studies are made on its application to large complicated parts whose substitution has been considered difficult.

**[0003]** Making such parts from nylon resin needs not only individual molding technologies (such as injection molding, extrusion molding and blow molding) but also post-processing technologies (such as cutting, bonding and welding) in combination. Unfortunately, conventional nylon resin compositions are formulated without post-processing being taken into account. If two or more parts of glass-reinforced nylon resin are to be welded together (by vibration welding or injection welding) to form a composite part of desired shape, it is difficult to achieve the desired level of strength in the weld zone. This is true particularly with large parts. Thus the use of nylon resin has been limited.

**[0004]** A first problem addressed by the present invention is to provide a weldable nylon resin composition which gives molded items without posing a problem of weld strength and a second problem is to provide a weldable nylon resin composition for production of molded items with intricately curved welding surfaces, especially while, at the same time, ensuring high weld strength.

**[0005]** A third problem addressed by the present invention is to provide a weldable nylon resin composition which yields molded items with high weld strength while retaining nylon's inherent characteristics such as good moldability, heat resistance, toughness, oil and gasoline resistance, wear resistance and surface smoothness.

**[0006]** According to a first aspect, the present invention provides a weldable resin composition which comprises 100 parts by weight of nylon resin as component (A), 0.1-50 parts by weight of polyolefin resin as component (B), and 10-150 parts by weight of glass fiber as component (C) blended together.

**[0007]** According to a second aspect, the present invention provides a process for producing a weldable resin composition, which process comprises melt-blending together 100 parts by weight of nylon resin as component (A), 0.1-50 parts by weight of polyolefin resin as component (B), 10-150 parts by weight of glass fiber as component (C), 0-3 parts by weight of a copper compound as component (D) and 0-5 parts by weight of a silicone compound as component (E). This embodiment may be modified such that the components (A), (C), (D), and (E) are melt-blended together and the resulting composition is subsequently incorporated with the component (B).

**[0008]** Additional aspects of the present invention include a molded item made of the weldable resin composition, a method of producing a molded product by welding from more than one molded item made of the weldable resin composition, and a molded product produced by the method.

**[0009]** Preferred embodiments of the invention will now be described.

**[0010]** In the following description, "weight" means "mass". The term "welding" means a process for melting the respective contact surfaces of molded items such that the molten surfaces bond together. Welding may be accomplished by, for example, vibration welding, ultrasonic welding, spin welding, injection welding, microwave welding, (RF induction welding), hot plate welding or hot air welding. Of these welding methods, vibration welding, injection welding (with the die sliding or rotating), ultrasonic welding and microwave welding are particularly desirable. Among them, vibration welding is the most desirable because of its good balance between high strength and easy processing.

**[0011]** Component (A) used in a composition embodying the present invention is a nylon resin, which is a polyamide derived at least mainly from dicarboxylic acid and any of amino acid, lactam, and diamine.

**[0012]** Typical examples of the major constituents are listed below.

- Amino acids such as 6-aminocaproic acid, 11-aminoundecanoic acid, 12-aminododecanoic acid and p-aminomethyl benzoic acid.
- Lactams such as  $\epsilon$ -caprolactam and  $\omega$ -laurolactam.
- Aliphatic, alicyclic and aromatic diamines, such as tetramethylenediamine, hexamethylenediamine, 2-methylpentamethylenediamine, nonamethylenediamine, undecamethylenediamine, dodecamethylenediamine, 2,2',4'- and/or 2,4,4'-trimethylhexamethylenediamine, 5-methylnonamethylenediamine, m-xylylenediamine, p-xylylenediamine, 1,3-bis(aminomethyl)cyclohexane, 1,4-bis(aminomethyl)cyclohexane, 1-amino-3-aminomethyl-3,5,5-trimethylcyclohexane, bis(4-aminocyclohexyl)methane, bis(3-methyl-4-aminocyclohexyl)methane, 2,2-bis(4-aminocyclohexyl)propane, bis(aminopropyl)piperazine and aminoethylpiperazine.
- Aliphatic, alicyclic, and aromatic dicarboxylic acids, such as adipic acid, suberic acid, azelaic acid, sebacic acid,

dodecanoic acid, terephthalic acid, isophthalic acid, 2-chloroterephthalic acid, 2-methylterephthalic acid, 5-methylisophthalic acid, 5-sodium sulfoisophthalic acid, hexahydroterephthalic acid and hexahydroisophthalic acid

**[0013]** The nylon resin used in a composition embodying the present invention may be a homopolymer or copolymer produced from these raw materials. Such polymers may be used alone or in combination with one another.

**[0014]** The nylon resin preferably has a melting point higher than 200°C so that it has good heat resistance and high strength. Typical examples of the nylon resin are listed below.

**[0015]** Polycaproamide (nylon 6), polyhexamethylene adipamide (nylon 66), polycaproamide/polyhexamethylene adipamide copolymer (nylon 6/66), polytetramethylene adipamide (nylon 46), polyhexamethylene sebacamide (nylon 610), polyhexamethylene dodecamide (nylon 612), polyhexamethylene terephthalamide/polycaproamide copolymer (nylon 6T/6), polyhexamethylene adipamide/polyhexamethylene terephthalamide copolymer (nylon 66/6T), polyhexamethylene adipamide/polyhexamethylene isophthalamide copolymer (nylon 66/6I), polyhexamethylene adipamide/polyhexamethylene terephthalamide/polyhexamethylene isophthalamide copolymer (nylon 66/6T/6I), polyhexamethylene terephthalamide/polyhexamethylene isophthalamide copolymer (nylon 6T/6I), polyhexamethylene terephthalamide/polydodecanamide copolymer (nylon 6T/12), polyhexamethylene terephthalamide/poly(2-methylpentamethylene)terephthalamide copolymer (nylon 6T/M5T), polyxylylene adipamide (nylon XD6), and polynonylamethylene terephthalamide (nylon 9T). They may be used in the form of blends or copolymers.

**[0016]** Preferable among these examples are nylon 6, nylon 66, nylon 6/66 copolymer, copolymer nylon composed mainly (i.e. at least 50 wt%) of nylon 6 or nylon 66, nylon 610, and copolymers (such as nylon 6T/66 copolymer, nylon 6T/6I copolymer, and nylon 6T/6 copolymer) having hexamethylene terephthalamide units. Nylon 6, nylon 66, and copolymers thereof are most desirable.

**[0017]** Two or more kinds of these nylon resins may be used so as to impart their characteristic properties, such as moldability, heat resistance and weldability. A desirable nylon resin composition consists, by wt% of the total nylon resin, of 99-50 wt% of component (a) and 1-50 wt% (preferably 15-30 wt%) of component (b), where component (a) is at least one kind of nylon resin selected from nylon 66, nylon 6, and nylon copolymer composed mainly of them, and component (b) is at least one kind of nylon resin other than mentioned above (selected from higher nylons such as nylon 610 and nylon 612 and semiaromatic nylons such as nylon 6T/6, nylon 6T/12, nylon 6T/66, nylon 66/6I, nylon 66/6T/6I, nylon 6T/6I and nylon 6T/M5T). Such a composition is desirable from the standpoint of improved weldability.

**[0018]** These nylon resins desirably have a degree of polymerization such as to provide a relative viscosity of 1.5-5.0, particularly 2.0-4.0 (measured for 1% solution in 98% conc. sulfuric acid at 25°C).

**[0019]** Component (B) used in a composition embodying the present invention is a polyolefin skeleton in the main chain. It may be selected so that it adequately controls the melt viscosity of the resulting resin composition. For example, it may be crystalline or amorphous or a composition thereof. It may be a homopolymer of unsaturated monomer or a copolymer of more than one monomer or a composition thereof. The copolymer may be a random copolymer or a block copolymer or a composition thereof.

**[0020]** Examples of the polyolefin resin as component (B) are listed below.

- Homopolymers such as polyethylene, polypropylene, polystyrene, polyacrylate ester, polymethacrylate ester, poly-1-butene, poly-1-pentene, and polymethylpentene.
- Ethylene- $\alpha$ -olefin copolymers.
- Homopolymers of vinyl alcohol ester.
- Polymers obtained by partial or whole hydrolysis of homopolymer of vinyl alcohol ester [polymer obtained by partial or whole hydrolysis of copolymer of (ethylene and/or propylene) and vinyl alcohol ester].
- Copolymers of (ethylene and/or propylene) and (unsaturated carboxylic acid and/or unsaturated carboxylic ester), such as copolymer of ethylene and (meth)acrylic acid and copolymer of ethylene, (meth)acrylic acid, and (meth)acrylic ester.
- Copolymers of (ethylene and/or propylene) and (unsaturated carboxylic acid and/or unsaturated carboxylic ester), with its carboxylic groups at least partly neutralized to form a metal salt, such as ethylene-(meth)acrylic acid copolymer, with its carboxylic groups at least partly neutralized to form a metal salt, and ethylene-(meth)acrylic acid-(meth)acrylic ester copolymer, with its carboxylic groups at least partly neutralized to form a metal salt.
- Block copolymers of conjugated diene and vinyl aromatic hydrocarbon.
- Hydrogenated products of such block copolymers.

**[0021]** Preferable among these examples are polyethylene, polypropylene, polyacrylate ester, polymethacrylate ester, ethylene- $\alpha$ -olefin copolymer, a copolymer of (ethylene and/or propylene) and (unsaturated carboxylic acid and/or unsaturated carboxylic ester), with its carboxylic groups at least partly neutralized to form a metal salt, block copolymers of conjugated diene and vinyl aromatic hydrocarbon, and hydrogenated products of such block copolymers. Polyethylene and ethylene- $\alpha$ -olefin copolymers are particularly desirable.

**[0022]** The ethylene- $\alpha$ -olefin copolymer is preferably derived from ethylene and at least one kind of  $\alpha$ -olefin having 3-20 carbon atoms and is preferably derived from ethylene and at least one kind of  $\alpha$ -olefin having 3-12 carbon atoms. This copolymer effectively contributes to mechanical strength and modification.

**[0023]** Examples of the  $\alpha$ -olefin having 3-20 carbon atoms include propylene, 1-butene, 1-pentene, 1-hexene, 1-heptene, 1-octene, 1-nonene, 1-decene, 1-undecene, 1-dodecene, 1-tridecene, 1-tetradecene, 1-pentadecene, 1-hexadecene, 1-heptadecene, 1-octadecene, 1-nonadecene, 1-eicosene, 3-methyl-1-butene, 3-methyl-1-pentene, 3-ethyl-1-pentene, 4-methyl-1-pentene, 4-methyl-1-hexene, 4,4-dimethyl-1-hexene, 4,4-dimethyl-1-pentene, 4-ethyl-1-hexene, 3-ethyl-1-hexene, 9-methyl-1-decene, 11-methyl-1-dodecene, and 12-ethyl-1-tetradecene. They may be used alone or in combination with one another.

**[0024]** The ethylene- $\alpha$ -olefin copolymer preferably contains  $\alpha$ -olefin comonomer in an amount of 1-30 mol%, more preferably 2-25 mol%, still more preferably 3-20 mol%. The copolymer may additionally contain at least one comonomer such as 1,4-hexadiene, dicyclopentadiene, 2,5-norbornadiene, 5-ethylidenenorbornane, 5-ethyl-2,5-norbornadiene and 5-(1'-propenyl)-2-norbornene.

**[0025]** The copolymer of (ethylene and/or propylene) and (unsaturated carboxylic acid and/or unsaturated carboxylic ester) may contain as the unsaturated carboxylic acid either acrylic acid or methacrylic acid or a mixture thereof and also contain as the unsaturated carboxylic ester their methyl ester, ethyl ester, propyl ester, butyl ester, pentyl ester, hexyl ester, heptyl ester, octyl ester, nonyl ester, or decyl ester, or a mixture thereof. Preferable among these copolymers are ethylene-methacrylic acid copolymer and ethylene-methacrylic acid-acrylic ester copolymer.

**[0026]** As for the copolymer of (ethylene and/or propylene) and (unsaturated carboxylic acid and/or unsaturated carboxylic ester), with its carboxylic groups at least partly neutralized to form a metal salt, the species of metal that may be used are alkali metals (such as Li, Na, K, Mg, Ca, Sr and Ba) and alkali earth metals (such as Al, Sn, Sb, Ti, Mn, Fe, Ni, Cu, Zn, and Cd). Of these metals, Zn is most desirable.

**[0027]** The block copolymer of conjugated diene and vinyl aromatic hydrocarbon denotes any block copolymer elastomer of A-B type or A-B-A' type, with the terminal blocks A and A' being the same or different and the aromatic moiety being monocyclic or polycyclic. It is a thermoplastic homopolymer or copolymer derived from a vinyl aromatic hydrocarbon, which is exemplified by styrene,  $\alpha$ -methylstyrene, vinyltoluene, vinylxylene, ethylvinylxylene and vinylnaphthalene, and mixture thereof. Block B is a polymer derived from a conjugated diene hydrocarbon which is exemplified by 1,3-butadiene, 2,3-dimethylbutadiene, isoprene and 1,3-pentadiene, and a mixture thereof. Alternatively, block B may be hydrogenated product.

**[0028]** The polyolefin resin as component (B) in a composition embodying the present invention is preferably a modified polyolefin resin which is obtained by modifying the above-mentioned polyolefin resin with at least one compound selected from unsaturated carboxylic acids and derivatives thereof. Such a modified polyolefin resin is characterized by its improved compatibility and ability to increase weld strength with a small amount added.

**[0029]** The modifier may be a derivative of an unsaturated carboxylic acid in the form of a metal salt, ester, imide or acid anhydride.

**[0030]** Examples of the unsaturated carboxylic acid and derivative thereof are listed below.

- Acrylic acid, methacrylic acid, maleic acid, fumaric acid, itaconic acid, crotonic acid, methylmaleic acid, methylfumaric acid, mesaconic acid, citraconic acid and glutaric acid, and metal salts thereof.
- Methyl hydrogen maleate, methyl hydrogen itaconate, methyl acrylate, ethyl acrylate, butyl acrylate, 2-ethylhexyl acrylate, hydroxyethyl acrylate, methyl methacrylate, 2-ethylhexyl methacrylate, hydroxyethyl methacrylate, aminoethyl methacrylate, dimethyl maleate, and dimethyl itaconate.
- Maleic anhydride, itaconic anhydride, citraconic anhydride, endobicyclo(2,2,1)-5-heptene-2,3-dicarboxylic acid and endobicyclo-(2,2,1)-5-heptene-2,3-dicarboxylic anhydride.
- Maleimide, N-ethylmaleimide, N-butylmaleimide and N-phenylmaleimide.
- Glycidyl acrylate, glycidyl methacrylate, glycidyl ethacrylate, glycidyl itaconate and glycidyl citraconate.
- 5-norbornene-2,3-dicarboxylic acid.

**[0031]** Of these examples, unsaturated dicarboxylic acids and acid anhydrides thereof are preferred. Maleic acid and maleic anhydride are particularly suitable.

**[0032]** The functional group-containing component may be incorporated into the olefin compound by, for example, copolymerization of an olefin compound (as the major constituent) with a functional group-containing olefin compound. Another way is by the grafting of an unmodified polyolefin with a functional group-containing olefin compound with the aid of a radical initiator. The amount of the functional group-containing component is preferably 0.001-40 mol%, more preferably 0.01-35 mol%, of the total amount of olefin monomer in the modified polyolefin.

**[0033]** The polyolefin resin as component (B) in a composition embodying the present invention may be produced, for example, by radical polymerization, coordination polymerization with the aid of a Ziegler-Natta catalyst, anionic polymerization, or coordination polymerization with the aid of a metallocene catalyst.

**[0034]** The amount of polyolefin resin as component (B) for 100 parts by weight of the nylon resin as component (A) is 0.1-50 parts by weight, preferably 0.1-30 parts by weight, and more preferably 0.5-30 parts by weight. With an amount less than 0.1 part by weight, the polyolefin resin does not contribute to improvement in weldability of the resin composition. With an amount more than 50 parts by weight, the polyolefin resin produces an adverse effect, such as decrease in flowability at the time of melt molding and decrease in heat resistance and mechanical strength.

**[0035]** The glass fiber as component (C) in the present invention may be one which is commonly used for resin reinforcement. It may be in the form of long fiber, short fiber (chopped strand), or milled fiber. The glass fiber is not specifically restricted in diameter. However, the fiber diameter usually ranges from 5 to 15  $\mu\text{m}$ . The glass fiber may or may not be coated with or sized with ethylene-vinyl acetate copolymer or thermosetting resin. The glass fiber is preferably coated with a surface treating agent such as silane coupling agent and titanate coupling agent. The amount of the glass fiber in the resin composition for 100 parts by weight of the nylon resins is 10-150 parts by weight, preferably 20-80 parts by weight, and more preferably 20-60 parts by weight.

**[0036]** The copper compound as component (D) which may be present in a composition embodying the present invention includes, for example, cuprous chloride, cupric chloride, cuprous bromide, cupric bromide, cuprous iodide, cupric iodide, cupric sulfate, cupric nitrate, copper phosphate, cuprous acetate, cupric acetate, cupric salicylate, cupric stearate and cupric benzoate. The inorganic copper halide mentioned above may form a complex compound with, for example, xylylene diamine, 2-mercaptobenzimidazole or benzimidazole. Of these examples, cuprous compounds are preferable, cuprous halides are more preferable, and cuprous acetate and cuprous iodide are most preferable.

**[0037]** The copper compound contributes to the strength of the weld zone when molded parts are joined together and the welded product undergoes annealing. The amount of the copper compound for 100 parts by weight of the nylon resin is preferably less than 3 parts by weight, for example 0.01-3 parts by weight, more preferably 0.015-2 parts by weight, still more preferably 0.02-2 parts by weight. With an amount less than 0.01 part by weight, the copper compound may not fully produce its effect. Conversely, with an amount more than 3 parts by weight, the copper compound may liberate metallic copper at the time of melt molding, causing discoloration which degrades the product value.

**[0038]** According to the present invention, the copper compound may be used in combination with an alkali halide compound. Examples of the alkali halide compound include lithium chloride, lithium bromide, lithium iodide, potassium chloride, potassium bromide, potassium iodide, sodium bromide and sodium iodide. Of these examples, potassium iodide and sodium iodide are particularly desirable. The amount of the alkali halide compound for 100 parts by weight of the nylon resin is preferably less than 5 parts by weight, for example, 0.01-5 parts by weight, more preferably 0.05-3 parts by weight.

**[0039]** The silicone compound as component (E) which may be present in a composition embodying the present invention is an organosilicone compound whose skeleton is a siloxane linkage having organic groups attached directly to silicon atoms therein. Examples of the organic group include a methyl group, ethyl group, phenyl group, vinyl group, and trifluoropropyl group. Any known silicone compounds may be used. Incidentally, the organic group may be partly substituted with an epoxy group, amino group, polyether group, carboxyl group, mercapto group, ester group, chloroalkyl group, hydroxyl group or alkyl group having 3 or more carbon atoms.

**[0040]** Silicone compounds are classified into silicone oil, silicone elastomer, and silicone resin according to the degree of crosslinking (see "Silicone Material Handbook" by Toray-Dow Corning Co., Ltd., August 1993.) Any of these may be used in a composition embodying the present invention.

**[0041]** Preferred examples of the silicone compounds include dimethyl silicone oil, phenylmethyl silicone oil, alkyl-modified silicone oil, fluorosilicone oil, polyether-modified silicone oil, aliphatic ester-modified silicone oil, amino-modified silicone oil, carboxylic acid-modified silicone oil, carbinol-modified silicone oil, epoxy-modified silicone oil, and mercapto-modified silicone oil. Additional examples include polyethylene glycol-modified silicone oil and polypropylene glycol-modified silicone oil, which contribute to weld strength. These silicone compounds may be used in combination with one another.

**[0042]** The amount of the silicone compound as component (E) for 100 parts by weight of the nylon resin as component (A) is preferably less than 5 parts by weight, for example, 0.1-5 parts by weight, more preferably 1-3 parts by weight.

**[0043]** The glass fiber specified above may be used in combination with other fibrous or non-fibrous inorganic fillers. Their Examples are listed below.

- Fibrous fillers such as carbon fiber, potassium titanate whisker, zinc oxide whisker, aluminum borate whisker, aramid fiber, alumina fiber, silicon carbide fiber, ceramic fiber, asbestos fiber, gypsum fiber and metal fiber.
- Silicates such as wollastonite, zeolite, sericite, kaolin, mica, clay, pyrophyllite, bentonite, asbestos, talc and alumina silicate.
- Metal compounds such as alumina, silicon oxide, magnesium oxide, zirconium oxide, titanium oxide and iron oxide.
- Carbonates such as calcium carbonate, magnesium carbonate and dolomite.
- Sulfates such as calcium sulfate and barium sulfate.

- Hydroxides such as magnesium hydroxide, calcium hydroxide and aluminum hydroxide.
- Non-fibrous fillers such as glass beads, ceramic beads, boron nitride, silicon carbide and silica, which may be hollow.

**[0044]** They may be used in combination with one another. These fibrous or non-fibrous fillers may be pretreated with an isocyanate compound, organosilane compound, organotitanate compound, organoborane compound or epoxy compound, so that they impart greater mechanical strength.

**[0045]** A nylon resin composition embodying the present invention may have incorporated in it, several additives as exemplified below.

- Nucleating agents such as talc, kaolin, organic phosphorus compound and polyether ether ketone
- Anti-coloring agents such as hypophosphite.
- Antioxidants such as hindered phenol and hindered amine.
- Slip agents such as polyalkylene glycol.
- Heat stabilizers, UV light stabilizers, and coloring agents.

**[0046]** A nylon resin composition embodying the present invention may be prepared, for example, in a particularly efficient way by melt-blending all the raw materials (such as nylon resin, polyolefin resin, and glass fiber, and optional copper compound and silicone compound) in a known melt blender (such as single- or twin-screw extruder, Banbury mixer, kneader, and mixing roll) at a temperature, say 220-330°C, selected according to the melting point of the nylon resin. This method may be modified such that the composition is prepared from all the raw materials except the polyolefin resin which (in the form of pellets) is added to the composition afterwards.

**[0047]** In this way a weldable resin composition embodying the present invention is obtainable which has a melt viscosity whose coefficient of shear rate dependence is higher than 1.05 and can exhibit outstanding weldability.

**[0048]** The coefficient of shear rate dependence is a value defined by "ratio of increase in melt viscosity at a low shear rate" divided by "ratio of increase in melt viscosity at a high shear rate". The "ratio of increase in melt viscosity at a low shear rate" is a value defined by "melt viscosity of the weldable resin composition at a low shear rate" divided by "melt viscosity of the weldable resin composition excluding component (B) at a low shear rate". The ratio of increase in melt viscosity at a high shear rate" is a value defined by "melt viscosity of the weldable resin composition at a high shear rate" divided by "melt viscosity of the weldable resin composition excluding component (B) at a high shear rate". The low shear rate is 60 sec<sup>-1</sup> and the high shear rate is 6000 sec<sup>-1</sup>. The melt viscosity (in poise) is measured under the following conditions. Equipment: Capillograph B1 made by Toyo Seiki Temperature: 20°C higher than the melting point of the nylon resin (in larger amount if two or more nylon resins are used). Residence time: 5 minutes Piston speed: 5 mm/min (for the shear rate of 60 sec<sup>-1</sup>) or 500 mm/min (for the shear rate of 6000 sec<sup>-1</sup>).

**[0049]** Incidentally, "the weldable resin composition excluding component (B)" denotes the resin composition which is composed of component (A) and component (C) and other optional components.

**[0050]** If the resin composition has a melt viscosity whose coefficient of shear rate dependence is high, it exhibits good flowability and hence good moldability at a high shear rate (which is normally encountered during injection molding) and it also increases in viscosity at a low shear rate (which is encountered during welding) and hence it exhibits high weld strength. Therefore, the resin composition preferably has a coefficient of shear rate dependence higher than 1.05, more preferably higher than 1.08, still more preferably higher than 1.10, so that it exhibits especially good practical weldability.

**[0051]** A weldable nylon resin compound embodying the present invention may be formed into weldable molded items by ordinary molding methods (such as injection molding, extrusion molding and blow molding) under ordinary molding conditions. The weldable molded items can be joined together to form a molded product of desired shape. They may have ribs on their welding surface so as to facilitate vibration welding, ultrasonic welding or microwave welding.

**[0052]** Welding of the weldable molded items may be accomplished in the following manner.

- Vibration welding: Two molded items are held together vertically such that their mating surfaces are pressed against each other, and they are subjected to vibration in the horizontal direction so that frictional heat for welding is generated at the mating surfaces. The frequency of vibration is 100-300 Hz and the amplitude of vibration is 0.5-2.0 mm.
- Injection welding: Molded items are inserted into a mold or moved in a mold, and the resin composition is injected into the space in which the joint is formed. The latter method is referred to as die slide molding or die rotating molding.
- Ultrasonic welding: Two molded items are held together vertically such that their mating surfaces are pressed against each other, and they are subjected to ultrasonic vibration in the vertical direction so that frictional heat for

welding is generated at the mating surfaces. The frequency of vibration is 100-300 Hz and the amplitude of vibration is 0.5-2.0 mm

- Microwave welding: Two molded items are held together such that their mating surfaces are pressed against each other, and they are subjected to high-frequency electric fields so that induction loss (due to friction among molecules) is produced and heat is generated for welding.

[0053] Using a welding method mentioned above, it is possible to produce welded products from resin compositions embodying the present invention. The resulting welded products are superior in weld strength, heat resistance, external appearance, dimensional and weld uniformity. Stable, high weld strength is the main advantage. Owing to this advantage, the welded products will find use in the field of automotive parts, such as air intake manifolds (for the intake system), water inlet and water outlets (for the cooling system), fuel injection and fuel delivery pipes (for the fuel system) and oil tanks and other vessels.

[0054] Preferred embodiments of the present invention will now be described in more detail with reference to the accompanying drawings and the following Examples.

[0055] In the accompanying drawings, Fig. 1 is a diagram showing the shape of a test piece used to evaluate the strength of vibration welding in the Examples. Parts A, B, C and D are a plan view, a front view, a right side view and a bottom view, respectively.

[0056] Fig. 2 is a diagram showing the shape of another test piece used to evaluate the strength of vibration welding in the Examples. Parts A, B and C are plan view, a front view and a right side view, respectively.

[0057] Fig. 3 is a diagram showing the shape of a hollow molded product obtained by vibration welding from the test pieces each shown in Fig. 1 and Fig. 2. Parts A, B and C are plan view, front view and right side view, respectively.

[0058] Fig. 4 is a plan view showing the shape of a test piece used to evaluate the strength of injection welding in the Examples.

[0059] Fig. 5 is a plan view showing the shape of a molded product formed from the test pieces shown in Fig. 4, which was used to evaluate the strength of injection welding in the Examples.

[0060] In the Examples and Comparative Examples, amounts are expressed in terms of parts by weight.

[0061] Strength of material, flowability and weld strength were measured by the methods explained below

#### (1) Strength of material:

Tensile strength : according to ASTM D638

Flexural modulus : according to ASTM D790

#### (2) Flowability:

A sample of the material is injected into a mold for spiral flow measurement (10 mm wide, 2 mm thick and 600 mm long) under the conditions specified below.

Injection temperature: 20°C higher than the melting point of the nylon (in larger amount if two or more nylon resins are used). Injection pressure: 30 kgf/cm<sup>2</sup>G

Mold temperature: 80°C

Flowability is expressed in terms of the length of the distance over which the injected melt has flowed in the mold. The longer the distance, the better the flowability.

#### (3) Weld strength (in the case of vibration welding)

Two test pieces each having a 1.5-mm wide mating surface and 2.5-mm high bead 1 are injection-molded under ordinary conditions as shown in Figs. 1 and 2. They are joined together at weld zone "a" by vibration welding under the following conditions by using a vibration welding machine, Model 2850, made by Branson Co., Ltd.

Frictional heat generated by vibration melts the bead, thereby giving a welded hollow product as shown in Fig. 3.

Clamp Pressure : 100 kgf

Frequency : 240 Hz

Amplitude : 1.5 mm

Melt down : 1.5 mm

The welded hollow product thus obtained is filled with water and subjected to internal pressure in a water tank. The pressure to bring about burst is regarded as weld strength.

The welded hollow product is kept at 150°C for 10 hours in a heating oven and then measured for weld strength in the same way as mentioned above. The retention of weld strength is calculated.

#### (4) Weld strength (in the case of injection welding)

Two test pieces (10 mm thick) are injection-molded under ordinary conditions as shown in Fig. 4. They are inserted into a mold for fatigue test samples and joined together by injection welding in such a way that the side 'a' constitutes the weld zone. The welded product thus obtained is subjected to tensile test (at a pulling rate of 5 mm/sec and a span of 50 mm). The force required to break the weld zone 'a' is regarded as weld strength.

The nylon resin and polyolefin resin used in the Examples and Comparative Examples are specified below

Nylon resin**[0062]**

N6 : nylon 6 resin having a melting point of 225°C and a relative viscosity of 2.70.  
 N6/66 : nylon 6/66 copolymer (97/3 in molar ratio) having a melting point of 217°C and a relative viscosity of 2.65  
 N66 : nylon 66 resin having a melting point of 265°C and a relative viscosity of 2.90  
 N610 : nylon 610 resin having a melting point of 225°C and a relative viscosity of 2.70  
 6T/12 : nylon 6T/12 copolymer (60/40 in molar ratio) having a melting point of 300°C and a relative viscosity of 2.50.

Polyolefin resin**[0063]**

B-1 : polypropylene (MFR = 1.5)  
 B-2 : modified polypropylene obtained from 100 parts by weight of B-1, 1 part by weight of maleic anhydride, and 0.1 part by weight of 2,5-dimethyl-2,5-di(tert-butylperoxy) hexane by melt extrusion through a twin-screw extruder at a cylinder temperature of 220°C.  
 B-3 : monomer of ethylene-methacrylic acid copolymer, with its carboxylic acid moiety partly forming a zinc salt.  
 B-4 : modified ethylene-1-butene copolymer obtained from 100 parts by weight of ethylene-1-butene copolymer, 1 part by weight of maleic anhydride, and 0.1 part by weight of 2,5-dimethyl-2,5-di(tert-butylperoxy) hexane by melt extrusion through a twin-screw extruder at a cylinder temperature of 230°C.  
 B-5 : modified low-density polyethylene obtained from 100 parts by weight of low-density polyethylene ( having a density of 0.905, produced with the aid of metallocene catalyst), 1 part by weight of maleic anhydride, and 0.1 parts by weight of 2,5-dimethyl-2,5-di(tert-butylperoxy)hexane by melt extrusion through a twin-screw extruder at a cylinder temperature of 230°C.

Examples 1 to 16 and Comparative Examples 1 to 4

**[0064]** Several compositions were made from nylon resin, polyolefin resin, glass fiber (13µm in diameter), and copper compound according to the formulations shown in Tables 1 to 5. Each composition was pelletized by melt blending through a twin-screw extruder (Model TEX30, made by The Japan Steel Works, Ltd.) at a cylinder temperature of 250-280°C and a screw speed of 150 rpm. The resulting pellets were dried and then injection molded (at a mold temperature of 80°C) into various test pieces. The pellet samples and test pieces were measured for melt viscosity, flowability, and strength. Hollow products were formed from test pieces by vibration welding, and they were tested for weld strength. The results are shown in Tables 1 to 5.

**[0065]** Incidentally, in Comparative Example 2, MAH-PPE denotes polyphenylene ether resin modified with maleic anhydride. The compound used as the heat resistant material is CuI (cuprous iodide) or KI (potassium iodide). The silicone compound is polypropylene glycol-modified silicone oil.

**[0066]** Examples 1 to 16 demonstrate that the weldable resin composition of the present invention has good flowability and material strength, which are balanced well with each other, and a melt viscosity whose coefficient of shear rate dependence is high. The resin composition gave, by vibration welding, hollow products having high weld strength.

**[0067]** In contrast, the resin compositions in Comparative Examples 1 to 4, which were not incorporated with a polyolefin resin, gave hollow products which are poor in weld strength and strength retention after annealing.

Table 1

	Item	Unit	Example 1	Example 2	Example 3	Example 4	Example 5
Formulation	Nylon resin (a)	-	N6	N6	N6	N6	N6
	Amount	pbw	100	100	100	100	100
	Polyolefin resin	-	B-1	B-2	B-3	B-4	B-5
	Amount	pbw	5	5	5	5	5
	Amount of glass fiber	pbw	45	45	45	45	45
Flowability	Length of flow	mm	150	145	150	145	148



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Table 1 (continued)

	Item	Unit	Example 1	Example 2	Example 3	Example 4	Example 5
	Material	Tensile strength	MPa	160	165	170	165
	strength	Flexural modulus	GPa	8.2	8.2	8.0	7.8
	Melt viscosity	at low shear rate	poise	12520	13700	12600	14910
		at high shear rate	poise	1710	1820	1700	1860
		Coefficient of shear rate dependence	-	1.05	1.08	1.06	1.15
	Weldability	Strenght of vibration welding	kgf/cm <sup>2</sup>	11.2	11.9	12.5	13.8
		After annealing (150°C, 10 h)	kgf/cm <sup>2</sup>	9.7	10.5	11.0	12.0
		Retention of strength	%	87	87	88	87

Table 2

	Item	Unit	Examples 6	Example 7	Example 8	Example 9	Example 10
	Formulation	Nylon resin (a)	-	N6	N6	N6	N6
		Amount	pbw	100	100	100	100
		Polyolefin resin	-	B-2	B-4	B-5	B-4
		Amount	pbw	2	10	10	15
		Amount glass fiber	pbw	45	45	45	50
		Copper compound	-		CuI/KI	CuI/KI	CuI/KI
		Amount	pbw	0.04/0.35	0.04/0.35	0.04/0.35	0.04/0.35
		Silicone compound	-	-	-	-	-
		Amount	pbw				1
	Flowability	Length of flow	mm	147	140	140	137
	Material	Tensile strength	MPa	170	165	165	160
	strength	Flexural modulus	GPa	8.0	7.5	7.5	7.0
	Melt viscosity	at low shear rate	poise	12000	15890	16120	17560
		at high shear rate	poise	1690	1900	1850	2000
		Coefficient of shear rate dependence	-	1.02	1.20	1.25	1.26

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Table 2 (continued)

	Item	Unit	Examples 6	Example 7	Example 8	Example 9	Example 10
5  10	Weldability						
	Strength of vibration welding	kgf/cm <sup>2</sup>	10.0	14.4	14.5	15.0	14.8
	After annealing (150°C, 10 h)	kgf/cm <sup>2</sup>	8.8	14.2	14.4	14.7	14.6
	Retention of strength	%	88	99	99	98	99

Table 3

	Item	Unit	Example 11	Example 12	Example 13	Example 14
20  25	Formulation					
	Nylon resin (a)	-	N66	N66	N66	N6/66
	Amount	pbw	100	100	100	100
	Polyolefin resin	-	B-4	B-5	B-4	B-4
	Amount	pbw	5	10	15	5
25  30	Amount of glass fiber	pbw	45	45	50	45
	Copper compound	-	CuI/KI	CuI/KI	CuI/KI	CuI/KI
	Amount	pbw	0.04/0.35	0.04/0.35	0.04/0.35	0.04/0.35
	Flowability					
	Length of flow	mm	150	150	145	145
30  35	Material strength					
	Tensile strength	MPa	180	180	174	155
	Flexural modulus	GPa	8.3	8.0	7.8	7.3
35  40	Melt viscosity					
	at low shear rate	poise	9300	9300	11050	11200
	at high shear rate	poise	1130	1100	1240	1300
	Coefficient of shear rate dependence	-	1.09	1.12	1.18	1.11
40  45	Weldability					
	Strength of vibration welding	kgf/cm <sup>2</sup>	10.0	11.3	12.1	13.4
	After annealing (150°C, 10 h)	kgf/cm <sup>2</sup>	10.0	11.2	11.8	13.4
	Retention of strength	%	100	99	98	100

Table 4

	Item	Unit	Example 15	Example 16
Formulation	Nylon resin (a)	-	N6	N66
	Amount	pbw	70	80
	Nylon resin (b)	-	N610	6T/12
	Amount	pbw	30	20
	Polyolefin resin	-	B-4	B-4
	Amount	pbw	5	5
	Amount of glass fiber	pbw	45	45
	Copper compound	-	CuI/KI	CuI/KI
	Amount	pbw	0.04/0.35	0.04/0.35
Flowability	Length of flow	mm	150	140
Material strength	Tensile strength	MPa	160	175
	Flexural modulus	GPa	7.2	8.5
Melt viscosity	at low shear rate	poise	13050	13780
	at high shear rate	poise	1600	1460
	Coefficient of shear rate dependence	-	1.17	1.25
Weldability	Strength of vibration welding	kgf/cm <sup>2</sup>	14.0	13.2
	After annealing (150°C, 10 h)	kgf/cm <sup>2</sup>	13.8	13.0
	Retention of strength	%	99	98

Table 5

	Item	Unit	Comparative Example 1	Comparative Example 2	Comparative Example 3	Comparative Example 4
Formulation	Nylon resin (a)	-	N6	N6	N66	N6/66
	Amount	pbw	100	100	100	100
	Other resin	-	-	MAH-PPE	-	-
	Amount	pbw	-	10	-	-
	Amount of glass fiber	pbw	45	45	45	45
Flowability	Length of flow	mm	150	138	155	150
Material strength	Tensile strength	MPa	170	165	180	158
	Flexural modulus	GPa	8.2	8.2	8.5	7.5

Table 5 (continued)

	Item	Unit	Comparative Example 1	Comparative Example 2	Comparative Example 3	Comparative Example 4
Melt viscosity	at low shear rate	poise	11430	15430	7550	8930
	at high shear rate	poise	1640	2150	1000	1150
	Coefficient of shear rate dependence	-	-	1.03	-	-
Weldability	Strength of vibration welding	kgf/cm <sup>2</sup>	9.0	8.5	7.5	9.4
	After annealing (150°C, 10 h)	kgf/cm <sup>2</sup>	7.8	7.6	6.0	7.7
	Retention of strength	%	87	89	80	82

Examples 17 and 18 and Comparative Examples 5 and 6

[0068] The same procedure as in Examples 1 to 16 was repeated except that the formulations were changed as shown in Table 6 and vibration welding was replaced by injection welding. The results are shown in Table 6. Incidentally, in Comparative Example 6, MAH-PPE denotes polyphenylene ether resin modified with maleic anhydride.

[0069] Examples 17 and 18 demonstrate that weldable resin compositions embodying the present invention have good flowability and material strength, which are balanced well with each other, and a melt viscosity whose coefficient of shear rate dependence is high. The resin composition gave, by injection welding, hollow products having high weld strength.

[0070] In contrast, the resin compositions in Comparative Examples 5 to 6, which were not incorporated with a polyolefin resin, gave hollow products which are poor in weld strength.

Table 6

	Item	Unit	Example 17	Example 18	Comparative Example 5	Comparative Example 6
Formulation	Nylon resin (a)	-	N6	N6	N6	N6
	Amount	pbw	100	100	100	100
	Polyolefin resin		B-4	B-5		
	Amount	pbw	5	5	-	-
	Other resin	-	-	-	-	MAH-PPE
	Amount	pbw				5
	Amount of glass fiber	pbw	45	45	45	45
Flowability	Length of flow	mm	145	148	150	138
Material strength	Tensile strength	MPa	165	165	170	165
	Flexural modulus	GPa	7.8	8.0	8.2	8.2

Table 6 (continued)

	Item	Unit	Example 17	Example 18	Comparative Example 5	Comparative Example 6
5	Melt viscosity	at low shear rate	poise	14910	14600	11430
		at high shear rate	poise	1860	1790	1640
		Coefficient of shear rate dependence	-	1.15	1.17	-
10						1.03
15	Weldability	Strength of injection welding	MPa	73	75	66
						58

### Claims

1. A weldable resin composition which comprises 100 parts by weight of a nylon resin as component (A), 0.1-50 parts by weight of a polyolefin resin as component (B) and 10-150 parts by weight of glass fiber as component (C) blended together.
2. A weldable resin composition according to Claim 1, which is capable of vibration welding, injection welding, ultrasonic welding or microwave welding.
3. A weldable resin composition according to Claim 2, which is capable of vibration welding.
4. A weldable resin composition according to any one of Claims 1 to 3, which has a melt viscosity whose coefficient of shear rate dependence is higher than 1.05.

Coefficient of shear rate dependence

= Ratio of increase in melt viscosity at a low shear rate /

Ratio of increase in melt viscosity at a high shear rate,

Ratio of increase in melt viscosity at a low shear rate

= Melt viscosity of the weldable resin composition at a low shear rate /

Melt viscosity of the weldable resin composition excluding

component (B) at a low shear rate,

Ratio of increase in melt viscosity at a high shear rate

= Melt viscosity of the weldable resin composition at a high shear rate /

Melt viscosity of the weldable resin composition excluding

component (B) at a high shear rate,

wherein the low shear rate is  $60 \text{ sec}^{-1}$  and the high shear rate is  $6000 \text{ sec}^{-1}$ .

5. A weldable resin composition according to any one of Claims 1 to 4 wherein the polyolefin resin as component (B) is at least one species selected from polyethylene, polypropylene, polyacrylic ester, polymethacrylic ester, ethylene- $\alpha$ -olefin copolymer, copolymer of (ethylene and/or propylene) and (unsaturated carboxylic acid and/or unsaturated carboxylic ester) with its carboxylic acid partly neutralized to form a metal salt, block copolymer of conjugated diene and vinyl aromatic hydrocarbon, and hydrogenated product of the block copolymer.
6. A weldable resin composition according to Claim 5, wherein the polyolefin resin as component (B) is polyethylene and/or ethylene- $\alpha$ -olefin copolymer.
7. A weldable resin composition according to Claim 6, wherein the polyolefin resin as component (B) is an ethylene- $\alpha$ -olefin copolymer in which the  $\alpha$ -olefin moiety is at least one species selected from  $\alpha$ -olefins having 3-20 carbon atoms and the amount of the comonomer is 1-30 mol%.
8. A weldable resin composition according to any one of Claims 1 to 7, wherein the polyolefin resin as component (B) is a modified polyolefin resin in which the modifier is at least one compound selected from unsaturated carboxylic acids and derivatives thereof.
9. A weldable resin composition according to Claim 8, wherein, in the modified polyolefin, the modifier is at least one compound selected from unsaturated carboxylic acids, metal salts thereof, esters thereof, amides thereof and acid anhydrides thereof.
10. A weldable resin composition according to any one of Claims 1 to 9, which further comprises 0.01-3 parts by weight of a copper compound as component (D) for 100 parts by weight of nylon resin.
11. A weldable resin composition according to Claim 10, wherein the copper compound is a cuprous compound.
12. A weldable resin composition according to Claim 11, wherein the cuprous compound is cuprous halide.
13. A weldable resin composition according to any one of Claims 1 to 12, which further comprises 0.1-5 parts by weight of a silicone compound as component (E) for 100 parts by weight of nylon resin.
14. A weldable resin composition according to any one of Claims 1 to 13, wherein the nylon resin is at least one species selected from nylon 66, nylon 6 and copolymers composed mainly of them.
15. A weldable resin composition according to Claim 14, wherein the nylon resin as component (A) is composed of (a) 99-50 wt% of at least one species selected from nylon 66, nylon 6, and copolymers composed mainly of them and (b) 1-50 wt% of at least one species selected from nylon resins other than (a) defined above.
16. A method of producing a weldable resin composition, which method comprises melt-blending 100 parts by weight of nylon resin as component (A), 0.1-50 parts by weight of polyolefin resin as component (B), 10-150 parts by weight of glass fiber as component (C), 0-3 parts by weight of a copper compound as component (D), and 0-5 parts by weight of a silicone compound as component (E), which method comprises melt-blending 100 parts by weight of nylon resin as component (A), 10-150 parts by weight of glass fiber as component (C), 0-3 parts by weight of a copper compound as component (D), and 0-5 parts by weight of a silicone compound as component (E), and then melt-blending the resulting composition with 0.1-50 parts by weight of polyolefin resin as component (B).
17. A molded product produced from a weldable resin composition as defined in any one of Claims 1 to 15.
18. A method of producing a molded product by welding two or more molded items each formed from a weldable resin composition as defined in any one of Claims 1 to 15.
19. A method according to Claim 18, wherein the molded product is hollow.
20. A molded product produced by a method as defined in Claim 18 or 19.

FIG.1

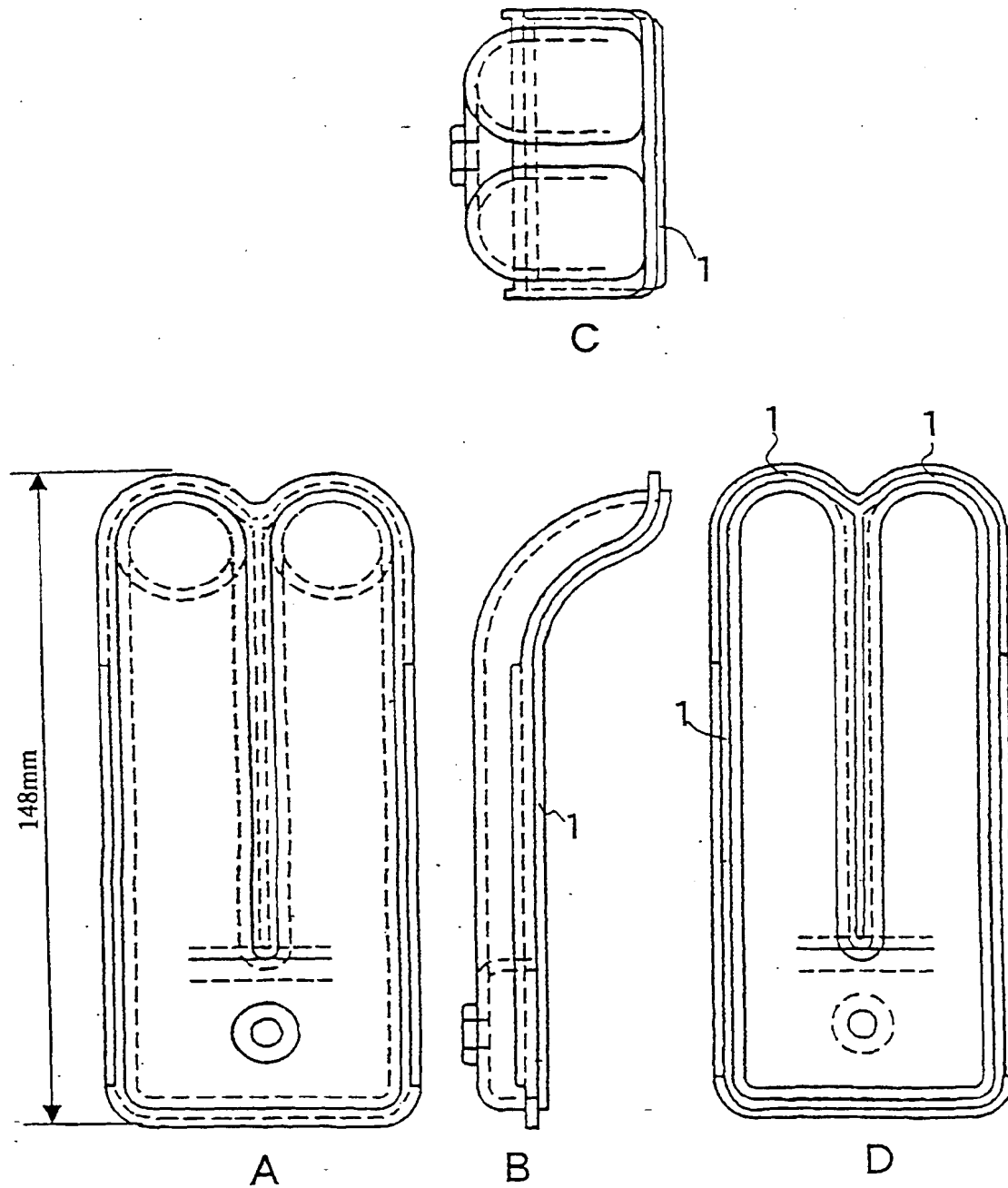


FIG.2

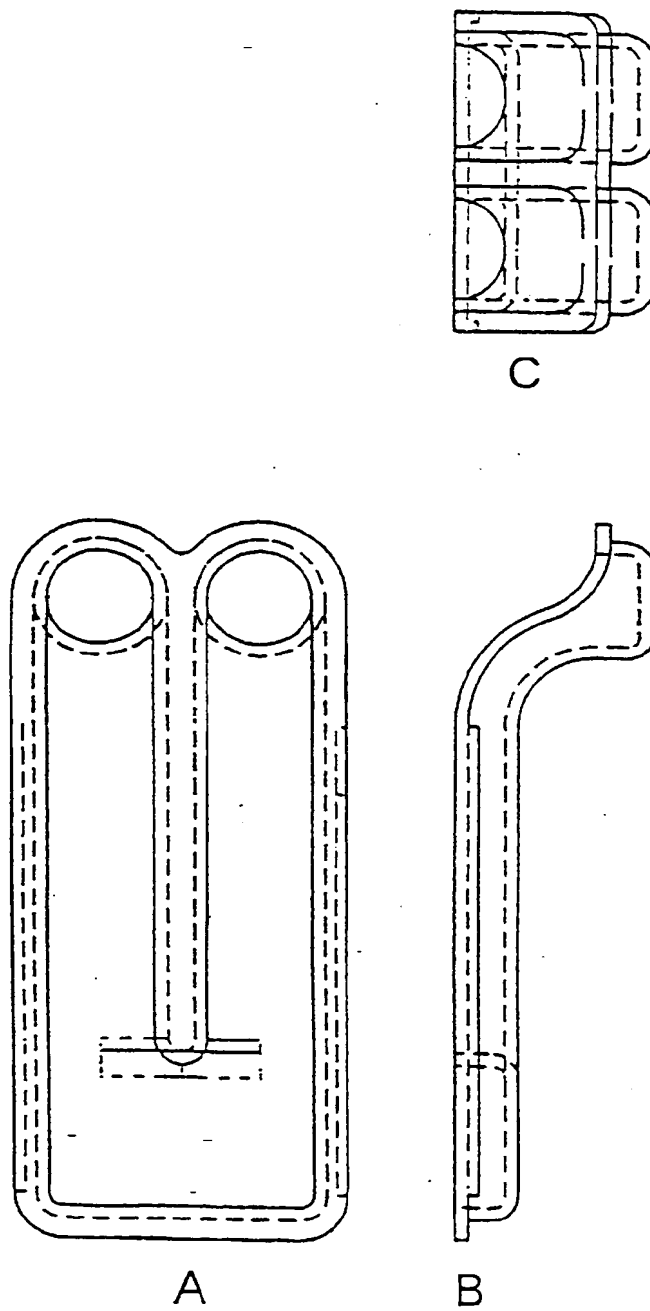




FIG.3

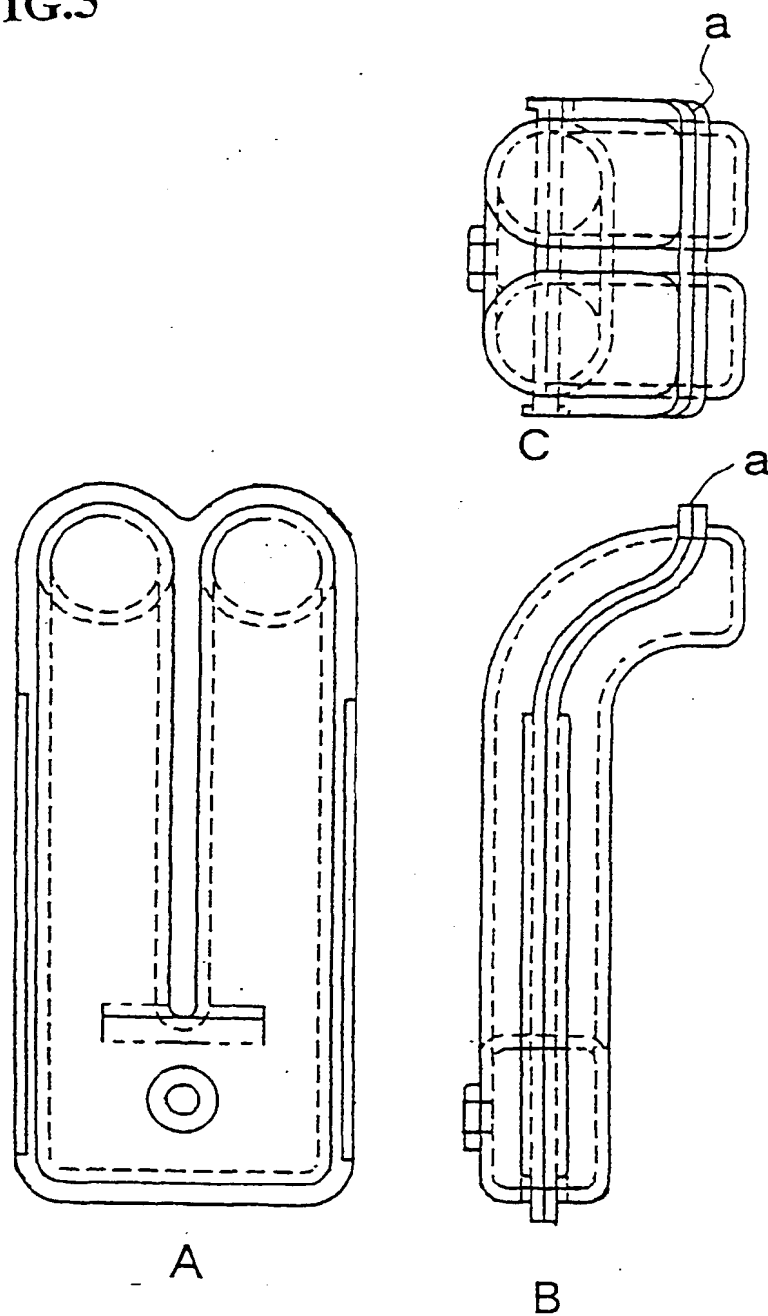


FIG.4

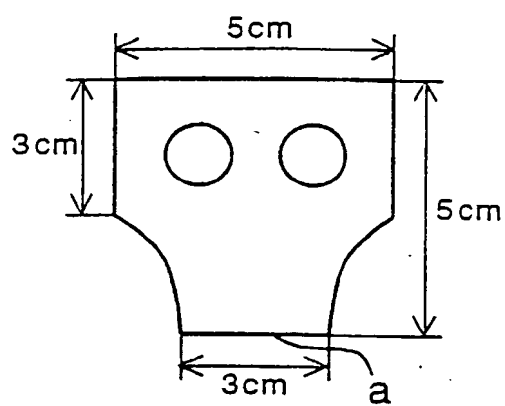
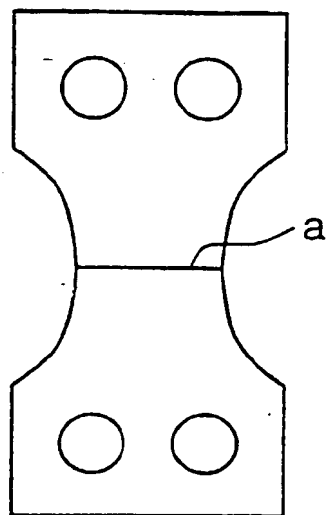


FIG.5





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# EUROPEAN SEARCH REPORT

Application Number  
EP 99 30 8397

## DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int Cl.7)
X	PATENT ABSTRACTS OF JAPAN vol. 1995, no. 02, 31 March 1995 (1995-03-31) & JP 06 322264 A (ASAHI (HEM IND CO LTD), 22 November 1994 (1994-11-22))	1,5,6,8, 9,14,15, 17-20	C08L77/00 B29C65/00
Y	* abstract *	1,10-12, 17-20	
X	PATENT ABSTRACTS OF JAPAN vol. 1998, no. 13, 30 November 1998 (1998-11-30) & JP 10 204286 A (TORAY IND INC), 4 August 1998 (1998-08-04) * abstract *	1	
Y	PATENT ABSTRACTS OF JAPAN vol. 1998, no. 14, 31 December 1998 (1998-12-31) & JP 10 231420 A (TORAY IND INC), 2 September 1998 (1998-09-02) * abstract *	1,10-12, 17-20	
X	US 4 174 358 A (EPSTEIN BENNETT N) 13 November 1979 (1979-11-13) * example 162 *	1,5,6,8, 9	C08L B29C
X	US 4 105 709 A (IWAMI ISAMU ET AL) 8 August 1978 (1978-08-08) * examples 3-5; table 4 *	1-3,5,8, 9	
X	EP 0 536 966 A (SUMITOMO CHEMICAL CO) 14 April 1993 (1993-04-14) * page 10, line 5-12, examples 3-6; tables 2,3 *	1-3,8,9, 14,16,17	
-/--			
The present search report has been drawn up for all claims			

TECHNICAL FIELDS  
SEARCHED (Int Cl.7)

Place of search

MUNICH

Date of completion of the search

18 January 2000

Examiner

Hutton, D

### CATEGORY OF CITED DOCUMENTS

- X particularly relevant if taken alone
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- A technical background
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- L document cited for other reasons
- S member of the same patent family, corresponding document

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# EUROPEAN SEARCH REPORT

Application Number  
EP 99 30 8397

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 7)
A	KAGAN V A ET AL. "OPTIMIZING THE VIBRATION WELDING OF GLASS-REINFORCED NYLON JOINTS" PLASTICS ENGINEERING, US. SOCIETY OF PLASTICS ENGINEERS, INC. GREENWICH, CONN. vol. 52, no. 9, page 39-41 XP000636014 ISSN: 0091-9578 ---	1.14, 17-20	
A	POTENTE H ET AL. "FRICTION WELDING OF POLYAMIDES" POLYMER ENGINEERING & SCIENCE, US. SOCIETY OF PLASTICS ENGINEERS, vol. 37, no. 4, page 726-737 XP000697920 ISSN: 0032-3888 ---	1.14, 17-20	
A	US 5 154 979 A (GAEHWILER HEINZ U ET AL) 13 October 1992 (1992-10-13) ---	1.2	
A	WO 97 17189 A (ALLIED SIGNAL INC) 15 May 1997 (1997-05-15) * the whole document *	1-20	
A	EP 0 540 842 A (DANUBIA PETROCHEM POLYMERE RENOLIT WERKE GES MIT BESCHRAE (DE); R) 12 May 1993 (1993-05-12) * the whole document * -----	1-3	
The present search report has been drawn up for all claims			
Place of search <b>MUNICH</b>		Date of completion of the search <b>18 January 2000</b>	Examiner <b>Hutton, D</b>
CATEGORY OF CITED DOCUMENTS		<ul style="list-style-type: none"> <li>- theory or principle underlying the invention</li> <li>E - earlier patent document, but published on or after the filing date</li> <li>D - document cited in the application</li> <li>L - document cited for other reasons</li> <li>3 - member of the same patent family, corresponding document</li> </ul>	
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EP 99 30 8397

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18-01-2000

Patent document cited in search report	Publication date	Patent family members	Publication date
JP 06322264 A	22-11-1994	NONE	
JP 10204286 A	04-08-1998	NONE	
JP 10231420 A	02-09-1998	NONE	
US 4174358 A	13-11-1979	CA 1133164 A CH 649566 A DE 2622973 A FR 2311814 A GB 1552352 A IT 1061385 B JP 1344392 C JP 51143061 A JP 55044108 B JP 1554624 C JP 59131649 A JP 63054308 B NL 7605495 A,B	05-10-1982 31-05-1985 09-12-1976 17-12-1976 12-09-1979 28-02-1983 29-10-1986 09-12-1976 10-11-1980 23-04-1990 28-07-1984 27-10-1988 25-11-1976
US 4105709 A	08-08-1978	JP 1005194 C JP 51125451 A JP 54004743 B CA 1063286 A DE 2613968 A FR 2306238 A GB 1491433 A	30-06-1980 01-11-1976 09-03-1979 25-09-1979 14-10-1976 29-10-1976 09-11-1977
EP 0536966 A	14-04-1993	CA 2079963 A DE 69219548 D DE 69219548 T JP 5239363 A US 5367013 A	10-04-1993 12-06-1997 04-09-1997 17-09-1993 22-11-1994
US 5154979 A	13-10-1992	DE 3911695 A AT 113977 T CA 2014099 A,C DE 59007665 D EP 0393409 A ES 2065426 T JP 2921581 B JP 3205429 A	11-10-1990 15-11-1994 10-10-1990 15-12-1994 24-10-1990 16-02-1995 19-07-1999 06-09-1991
WO 9717189 A	15-05-1997	EP 0859698 A	26-08-1998
EP 0540842 A	12-05-1993	AT 399158 B	27-03-1995

EP 0 997 496 A1

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ANNEX TO THE EUROPEAN SEARCH REPORT  
ON EUROPEAN PATENT APPLICATION NO.

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The members are as contained in the European Patent Office (EPO) file on  
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18-01-2000

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
EP 0540842 A		AT 183391 A	15-08-1994
		AT 140250 T	15-07-1996
		DE 69212114 D	14-08-1996
		DK 540842 T	12-08-1996
		ES 2089315 T	01-10-1996

EPO/EP 0540842

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